

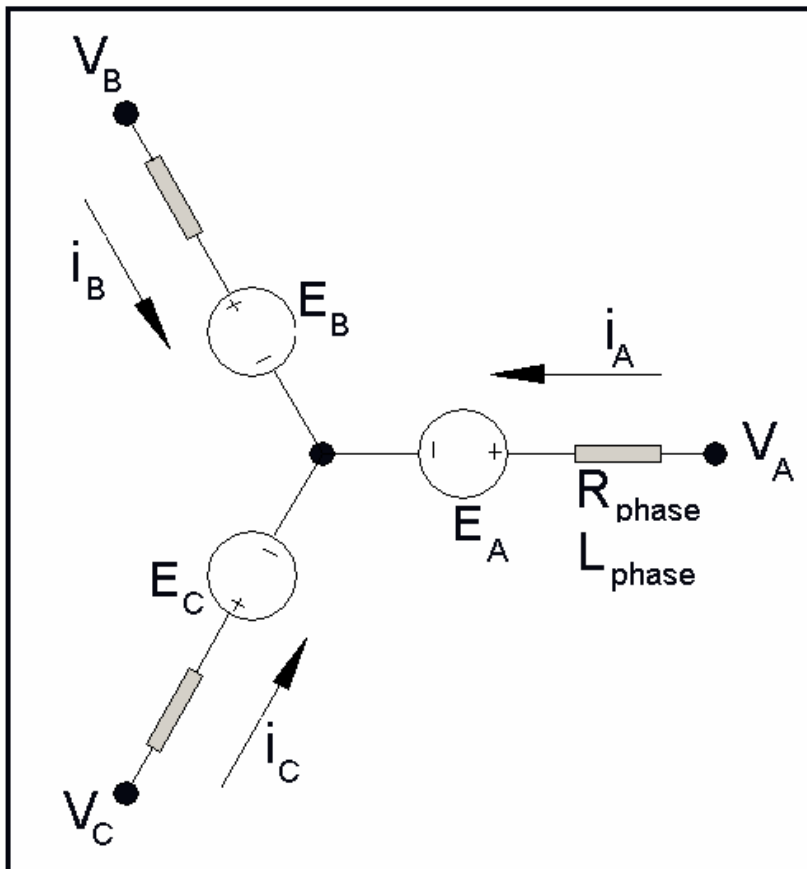
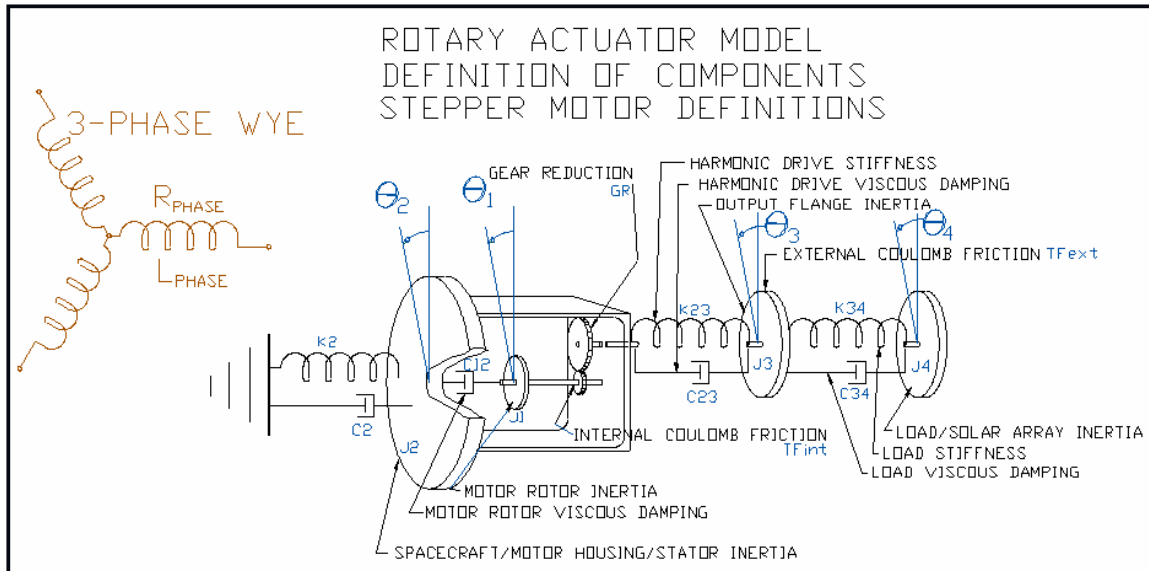
# 3-Phase Wye Stepper Motor Model

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## The Model

This is a 4 degree of freedom electro-mechanical math model representing the motor rotor, the spacecraft, the output flange, and the flexible load (solar array).



### Phase Torque Constants

$$K_{t\_phase} := \frac{2}{3} \cdot K_T \quad \begin{array}{l} \text{Maximum phase Torque constant} \\ \text{from overall motor } K_t, \text{ N-m/amp} \\ \text{1 leg to 2 leg standard operation} \end{array}$$

$$K_{t\_instA}(\theta) := K_{t\_phase} \cdot \sin\left(\frac{2 \cdot \pi}{6} \cdot \frac{\theta}{\text{Step\_size}}\right)$$

$$K_{t\_instB}(\theta) := K_{t\_phase} \cdot \sin\left(\frac{2 \cdot \pi}{6} \cdot \frac{\theta}{\text{Step\_size}} - \frac{4 \cdot \pi}{3}\right)$$

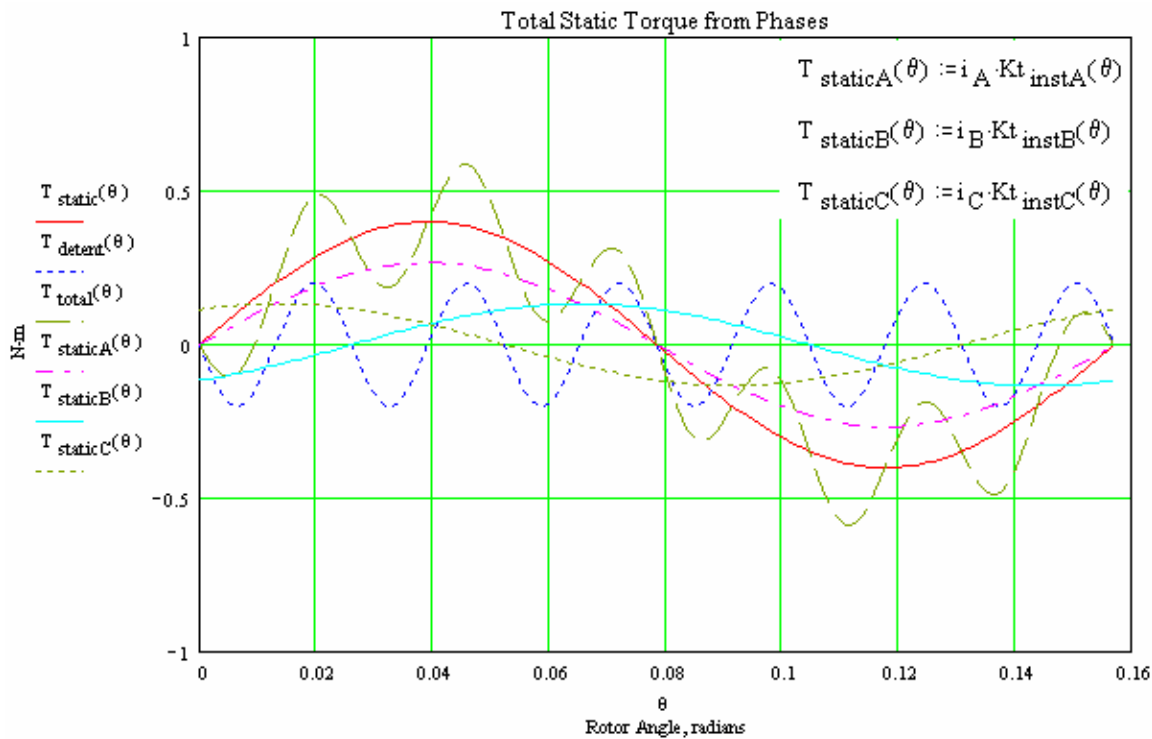
$$K_{t\_instC}(\theta) := K_{t\_phase} \cdot \sin\left(\frac{2 \cdot \pi}{6} \cdot \frac{\theta}{\text{Step\_size}} - \frac{2 \cdot \pi}{3}\right)$$

Theta  $\theta$  used here is the physical rotor angle, in the diagram =  $\theta_1$

The Step<sub>size</sub> for this motor = 1.5 degrees, or 0.026178 radians

### Detent Torque

$$T_{detent}(\theta) := -T_{detent\_max} \cdot \sin\left(\frac{2 \cdot \pi \cdot \theta}{\text{Step\_size}}\right)$$

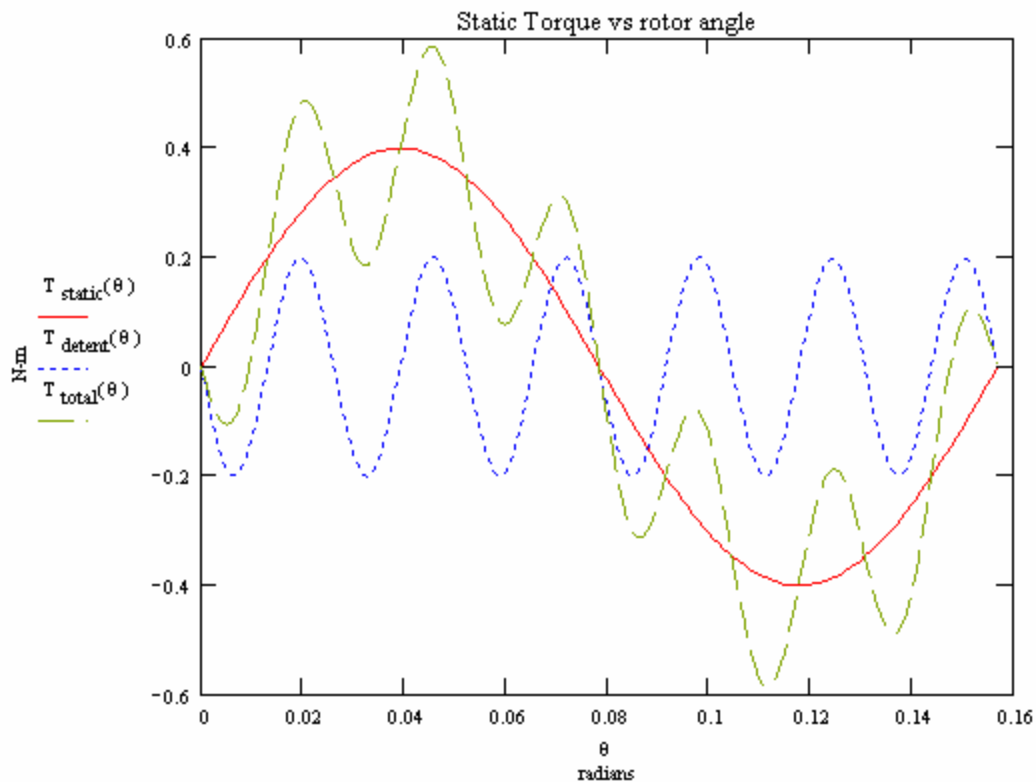


## Static Torque Curve

With no transient effects and no back-emf effects, this is the shape of the static torque curve for  $I_{\text{circuit}} = 0.2$  amps:

$$T_{\text{detent}}(\theta) := -T_{\text{detent\_max}} \cdot \sin\left(\frac{2 \cdot \pi \cdot \theta}{\text{Step\_size}}\right) \quad T_{\text{static}}(\theta) := I_{\text{circuit}} \cdot K_T \cdot \sin\left(\frac{2 \cdot \pi \cdot \theta}{6 \cdot \text{Step\_size}}\right)$$

$$T_{\text{total}}(\theta) := T_{\text{static}}(\theta) + T_{\text{detent}}(\theta)$$



Note the exaggerated effect of the detent when operating at such low currents.

## Motor Stiffness

$$\text{MotorStiffness}(\theta) := \frac{d}{d\theta} T_{\text{total}}(\theta) := \left( \frac{\pi}{3 \cdot \text{Step\_size}} \cdot I_{\text{circuit}} \cdot K_T \cdot \cos\left(\frac{1}{3} \cdot \pi \cdot \frac{\theta}{\text{Step\_size}}\right) \right) - \left( \frac{2 \cdot \pi}{\text{Step\_size}} \cdot T_{\text{detent\_max}} \cdot \cos\left(2 \cdot \pi \cdot \frac{\theta}{\text{Step\_size}}\right) \right)$$

$$\text{ReflectedStiffness}(\theta) := \text{MotorStiffness}(\theta) \cdot GR^2$$

With 0.2 amps the reflected motor stiffness at the gear head output (but before the flexible portion of the harmonic drive) =  $2.56 \times 10^6$  N-m/rad

Un-powered the reflected motor stiffness at the gear head output =  $1.92 \times 10^6$  N-m/rad

This is extremely stiff (100x stiffer) when compared to the harmonic drive.

### Back EMF voltage

A motor is also a generator, and generates a back voltage proportional to the speed of the rotor and the instantaneous value of the motor constant (which varies sinusoidally in a non-commutated motor such as a stepper motor).

$$E_A = -\frac{d\theta}{dt} \cdot Kt_{instA}$$

$$E_B = -\frac{d\theta}{dt} \cdot Kt_{instB}$$

$$E_C = -\frac{d\theta}{dt} \cdot Kt_{instC}$$

### Transient Calculation of Phase Currents

The inductance creates transient current effects for the applied voltage:  
The first 2 equations must be time-domain integrated.

$$\frac{di_A}{dt} = \frac{2 \cdot V_A - V_B - V_C}{3 \cdot L_{phase}} - \frac{R_{phase}}{L_{phase}} \cdot i_A + \frac{2 \cdot E_A - E_B - E_C}{3 \cdot L_{phase}}$$

$$\frac{di_B}{dt} = \frac{2 \cdot V_B - V_A - V_C}{3 \cdot L_{phase}} - \frac{R_{phase}}{L_{phase}} \cdot i_B + \frac{2 \cdot E_B - E_A - E_C}{3 \cdot L_{phase}}$$

$$i_C = -i_A - i_B$$

### Net Motor Torque

$$T_{electrical} = i_A \cdot Kt_{instA} + i_B \cdot Kt_{instB} + i_C \cdot Kt_{instC}$$

$$T_{NET} = T_{electrical} + T_{detent}$$

### Input Friction

Friction from the harmonic drive and motor bearings as a function of rotor speed and temperature, as seen by the motor rotor (N-m):

$$Tf_{int} = A_o + A_1 \cdot \left( \frac{d\theta_1}{dt} \right)^{A_2} \cdot 10^{A_3 \cdot (Temperature + A_4)}$$

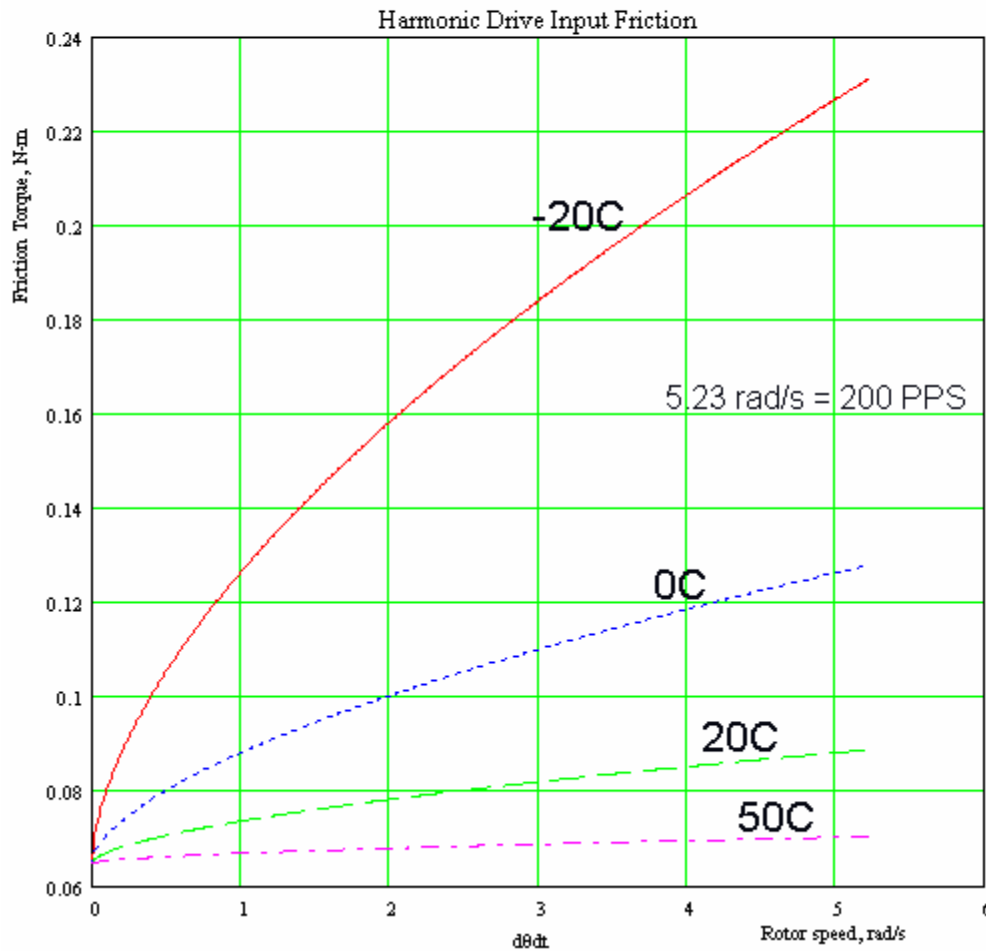
A<sub>o</sub> is the static break-away torque at room temperature (21°C)

Type 5 size Harmonic Drive Friction Map, friction torque Qinput

A<sub>o</sub> := 0.065      A<sub>1</sub> := 0.0345      A<sub>2</sub> := 0.6      A<sub>3</sub> := -0.021      A<sub>4</sub> := 8.0

dθ/dt is the rotor speed, radians per second

Temperature is the temperature in degC



## Differential Equations of Motion

Note: Internal friction force  $Tf_{int}$  is + when  $(d\theta_1/dt - d\theta_2/dt)$  is +  
 External friction force  $Tf_{ext}$  is + when  $(d\theta_3/dt - d\theta_2/dt)$  is +

Motor rotor

$$J_1 \cdot \frac{d^2\theta_1}{dt^2} = T_{NET} - Tf_{int}$$

$$- \frac{K_{23}}{GR} \cdot \left[ \frac{\theta_1}{GR} - \theta_2 \cdot \left( 1 + \frac{1}{GR} \right) + \theta_3 \right]$$

$$- \frac{C_{23}}{GR} \cdot \left[ \frac{d\theta_1}{dt} - \frac{d\theta_2}{dt} \cdot \left( 1 + \frac{1}{GR} \right) + \frac{d\theta_3}{dt} \right] - C_{12} \cdot \left( \frac{d\theta_1}{dt} - \frac{d\theta_2}{dt} \right)$$

Spacecraft

$$J_2 \cdot \frac{d^2\theta_2}{dt^2} = -T_{NET} + Tf_{int} + Tf_{ext} + T_{environmental} + T_{ReactionWheels}$$

$$+ K_{23} \cdot \left[ \frac{\theta_1}{GR} - \theta_2 \cdot \left( 1 + \frac{1}{GR} \right) + \theta_3 \right] \cdot \left( 1 + \frac{1}{GR} \right)$$

$$+ C_{23} \cdot \left[ \frac{d\theta_1}{dt} - \frac{d\theta_2}{dt} \cdot \left( 1 + \frac{1}{GR} \right) + \frac{d\theta_3}{dt} \right] \cdot \left( 1 + \frac{1}{GR} \right) + C_{12} \cdot \left( \frac{d\theta_1}{dt} - \frac{d\theta_2}{dt} \right)$$

Output Flange

$$J_3 \cdot \frac{d^2\theta_3}{dt^2} = -Tf_{ext}$$

$$- K_{23} \cdot \left[ \frac{\theta_1}{GR} - \theta_2 \cdot \left( 1 + \frac{1}{GR} \right) + \theta_3 \right] + K_{34} \cdot (\theta_4 - \theta_3)$$

$$- C_{23} \cdot \left[ \frac{d\theta_1}{dt} - \frac{d\theta_2}{dt} \cdot \left( 1 + \frac{1}{GR} \right) + \frac{d\theta_3}{dt} \right] + C_{34} \cdot \left( \frac{d\theta_4}{dt} - \frac{d\theta_3}{dt} \right)$$

Flexible Load (solar array)

$$J_4 \cdot \frac{d^2\theta_4}{dt^2} = -K_{34} \cdot (\theta_4 - \theta_3) - C_{34} \cdot \left( \frac{d\theta_4}{dt} - \frac{d\theta_3}{dt} \right)$$

*Stepper Motor States*

The power is switched so as to provide voltage to the phases according to the following state table:

STATE	Phase A	Phase B	Phase C
1	+	+	-
2	+	-	-
3	+	-	+
4	-	-	+
5	-	+	+
6	-	+	-